

Sequence Design Example for **Ultra-Wideband** **Impulse Radio** Using Maximal Length Sequences

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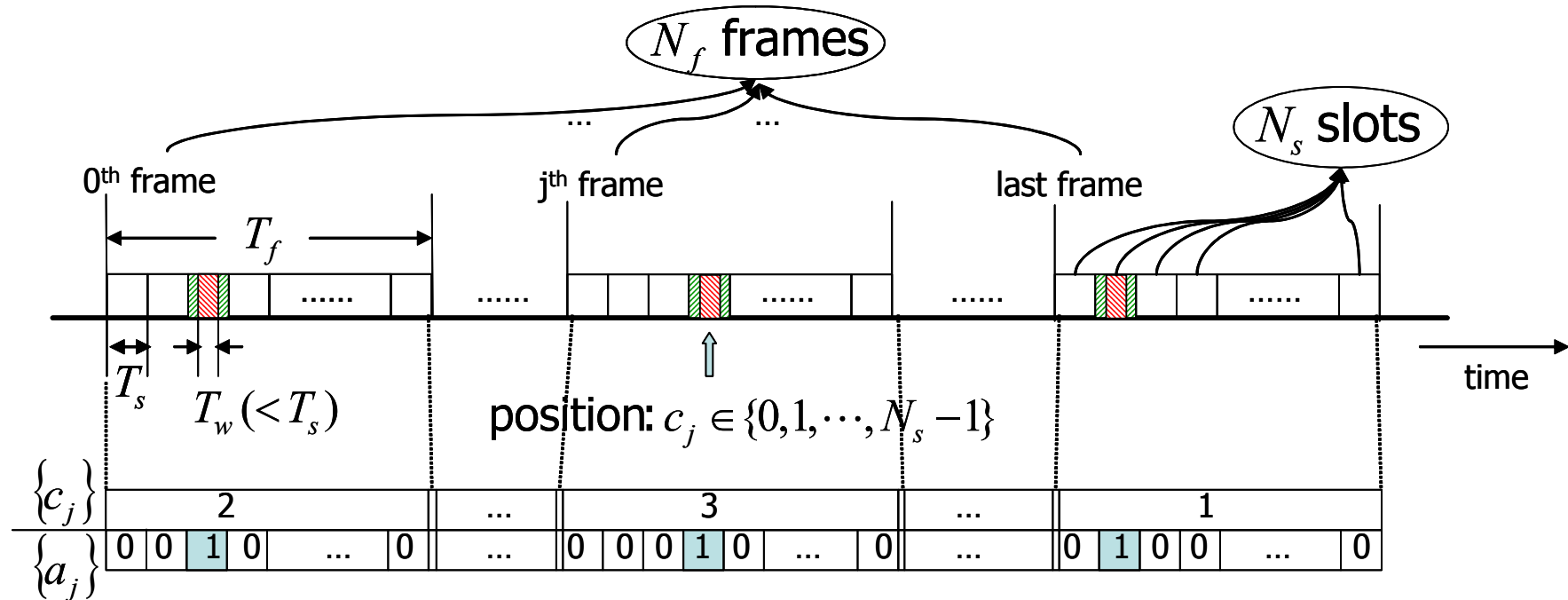


In this presentation ...



- General **signal model** for sequence designs suitable for UWB signals using TH-SSMA (Time Hopping Spread Spectrum Multiple Access)
- Sequence **construction**
- Analysis
 - **Correlation** measure
 - **Power Spectral Density (PSD)** Consideration

Signal Model



【Fig. 1】 Illustration of UWB Time-Hopping (Impulse Radio) signal models

T_s : slot width
 N_s : number of slots within one frame
 T_f : frame duration ($T_f = T_s \cdot N_s$)
 N_f : period of integer time-hopping code
 T_w : pulse width ($T_w < T_s$)



Time-Hopping Signal Models — (2)



- i^{th} (unmodulated) TH-UWB signal

$$s^{(i)}(t) = \sum_j p(t - jT_f - c_j^{(i)}T_s) = \sum_n a_n^{(i)} p(t - nT_s)$$

$\{c_j^{(i)}\}_{j=0}^{N_f-1}$: N_s - ary integer TH code of period N_f

$$\{a_n^{(i)}\}_{j=0}^{N_s N_f - 1} = \begin{cases} 1, & \text{if } \exists j \in \mathbb{Z} \text{ s.t } n = jN_s + c_j^{(i)} \\ 0, & \text{O.W.} \end{cases}$$

: binary representation of $c_j^{(i)}$ of period $N_s N_f$

- Normalized periodic crosscorrelation between user i and user k

$$\Lambda_{i,k}(n_\tau T_s) = \frac{1}{N_f} \sum_{n=0}^{N_s N_f - 1} a_n^{(i)} a_{n \oplus n_\tau}^{(k)} \quad (\text{c.f. divided by } N_f, \text{ NOT } N_s N_f)$$



Impulse Radio Sequence (IRS) — definition



● \mathbb{C} : $(N_s, N_f, \lambda_a, \lambda_c)$ -IRS

$\Leftrightarrow \mathbb{C}$: a family of $(0, 1)$ -sequences of *length* $N_s N_f$ and *weight* N_f such that

1) **Pulse position** property: for $\forall x = \{x_t\}_{t=0}^{N_s N_f - 1} \in \mathbb{C}$,

- ▶ $N_s N_f$ slots are uniformly divided into N_f frames
- ▶ Each frame has a unique pulse position among its N_s slots
- ▶ $\text{supp}(x) = \{c_j + jN_s \mid j = 0, 1, \dots, N_f - 1, c_j \in \mathbb{Z}_{N_s}\}$

2) **Autocorrelation** property: for $\forall x = \{x_t\}_{t=0}^{N_s N_f - 1} \in \mathbb{C}$ and $\forall \tau \not\equiv 0 \pmod{N_s N_f}$,

$$\sum_{t=0}^{N_s N_f - 1} x_t x_{t \oplus \tau} \leq \lambda_a$$

3) **Crosscorrelation** property: for $\forall x = \{x_t\}_{t=0}^{N_s N_f - 1} \in \mathbb{C}$, $\forall y = \{y_t\}_{t=0}^{N_s N_f - 1} \in \mathbb{C}$, $x \neq y$, $\forall \tau$,

$$\sum_{t=0}^{N_s N_f - 1} x_t y_{t \oplus \tau} \leq \lambda_c$$



Optimality in view of Correlation



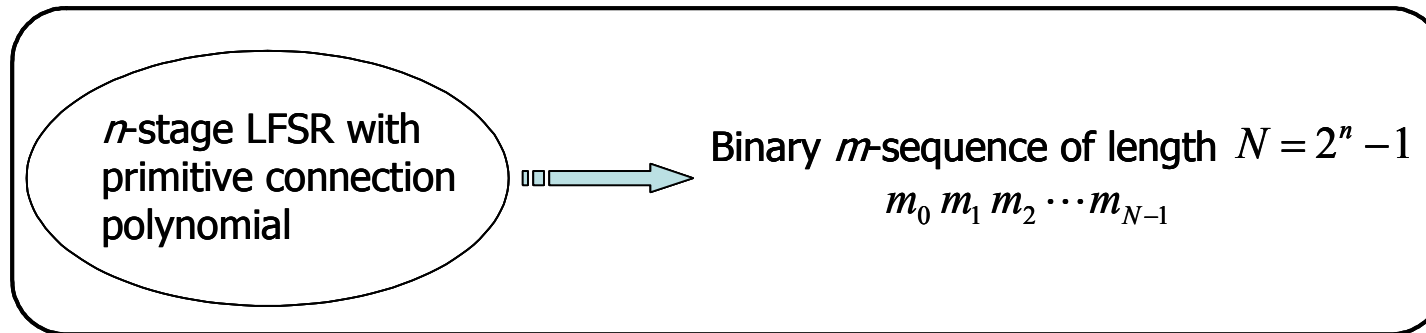
- For given parameters $N_s, N_f, \lambda_a, \lambda_c$
 - $\Phi(N_s, N_f, \lambda_a, \lambda_c)$ = the maximum cardinality of $(N_s, N_f, \lambda_a, \lambda_c) - IRS$
- Exact value of Φ is difficult to determine
 - ⇒ Need some bound (Johnson bound)
- **Johnson Bound**
 - **Upper bound** for $A(n, d; w)$
 - $A(n, d; w)$: maximum # of bin. vectors of length n , minimum distance $d_{\min} = d$, weight w
 - $A(n, 2\delta; w) \leq \left\lfloor \frac{n}{w} \left\lfloor \frac{n-1}{w-1} \dots \left\lfloor \frac{n-(w-\delta)}{\delta} \right\rfloor \dots \right\rfloor \right\rfloor$
 - When $\lambda_a = \lambda_c = \lambda$:

$$\Phi(N_s, N_f, \lambda) \leq \left\lfloor \frac{1}{N_f} \left\lfloor \frac{N_s N_f - 1}{N_f - 1} \dots \left\lfloor \frac{N_s N_f - \lambda}{N_f - \lambda} \right\rfloor \dots \right\rfloor \right\rfloor$$

Sequence

Construction

- Maximal length LFSR (Linear Feedback Shift Register) sequence (***m*-sequence**)



【Fig. 2】 Generator of binary maximal length sequences

- Properties of *m*-sequence

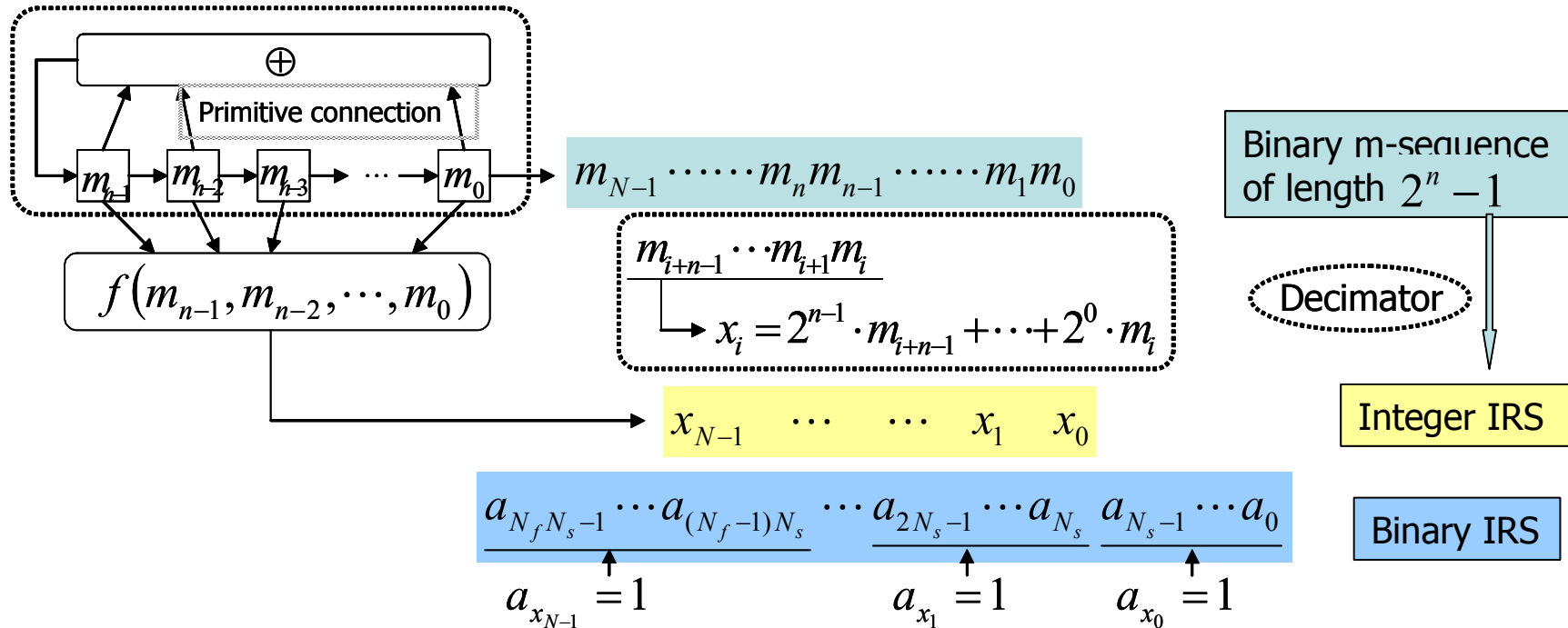
- *Maximal length* (period): $N = 2^n - 1$

- ***Ideal* (conventional) autocorrelation**: $R(\tau) = \begin{cases} -1, & \tau \not\equiv 0 \pmod{N} \\ N, & \tau \equiv 0 \pmod{N} \end{cases}$

- ***Span property***: N consecutive n -bits are all distinct, $m_i \cdots m_{i+n-1} \neq m_j \cdots m_{j+n-1}$

- ***Run property***, etc.

- Number of (cyclically) *distinct m*-sequence: $M_n = \frac{\phi(2^n - 1)}{n}$ ($\phi(\cdot)$ is Euler phi-function)



【Fig. 3】 Construction of proposed impulse radio sequences (Type I)

- There are $M_n = \phi(2^n - 1)/n$ cyclically distinct m-sequences.
- $(N_s, N_f, \lambda_a, \lambda_c) = \begin{cases} (2^n, 2^n - 1, \lambda_a, \lambda_c) & , \text{Type I} \\ (2^n - 1, 2^n - 1, \lambda_a, \lambda_c) & , \text{Type II} \end{cases}$ -IRS with M_n -sequences
 (Type II; $x_i \neq 0$ for all $i = 0, 1, \dots, N_f - 1$ by **span** property)

Analysis



Parameters and Correlation Property



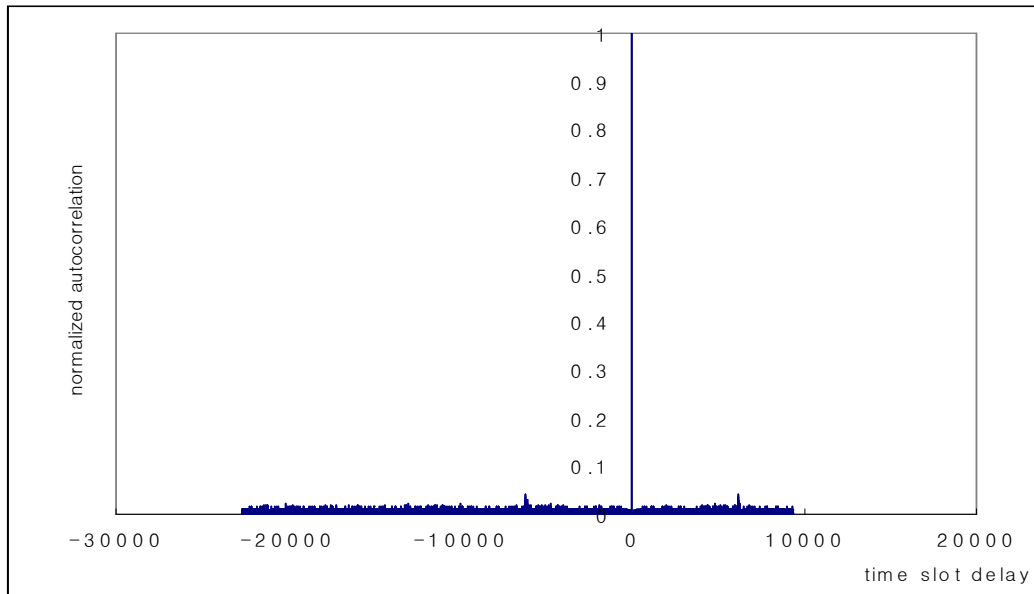
[Table 1] Parameters of proposed IRSs

n		3	4	5	6	7	8	9	10
Number of sequences		2	2	6	6	18	16	48	60
(N_s, N_f)	[3] with $l = n - 3$	N/A	N/A	(4, 15)	(8, 21)	(16, 31)	(32, 51)	(64, 85)	(128, 146)
	Type I	(8,7)	(16, 15)	(32, 31)	(64, 63)	(128, 127)	(256, 255)	(512, 511)	(1024, 1023)
	Type II	(7, 7)	(15, 15)	(31, 31)	(63, 63)	(127, 127)	(255, 255)	(511, 511)	(1023, 1023)
Period of Binary IRS: $(N_s \cdot N_f)$	[3]	N/A	N/A	60	168	496	1,632	5,440	18,688
	Type I	56	240	992	4032	16,256	65,280	261,632	1,047,552
	Type II	49	225	961	3969	16,129	65,025	261,121	1,046,529

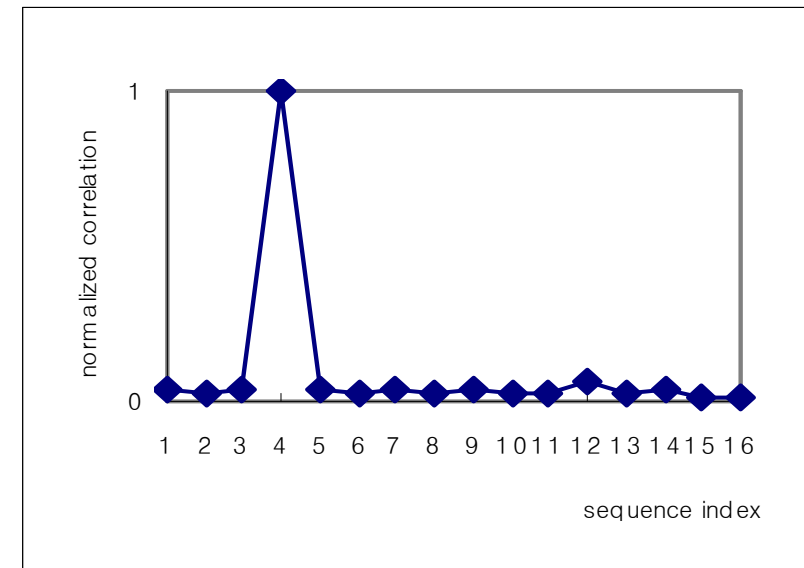
[Table 2] Correlation Properties of proposed IRS (Type I)

n		3	4	5	6	7	8	9	10
Autocorrelation (λ_a)	unnormalized $\max_i \max_{\tau \neq 0} R_{ii}(\tau)$	3	4	5	6	8	11	16	20
	normalized $\max_i \max_{\tau \neq 0} \widetilde{R}_{ii}(\tau)$	0.429	0.267	0.161	0.095	0.063	0.043	0.031	0.020
Crosscorrelation (λ_c)	unnormalized $\max_{i \neq j} \max_{\tau} R_{ij}(\tau)$	3	4	6	8	10	15	19	23
	normalized $\max_{i \neq j} \max_{\tau} \widetilde{R}_{ij}(\tau)$	0.429	0.267	0.193	0.127	0.079	0.059	0.037	0.022

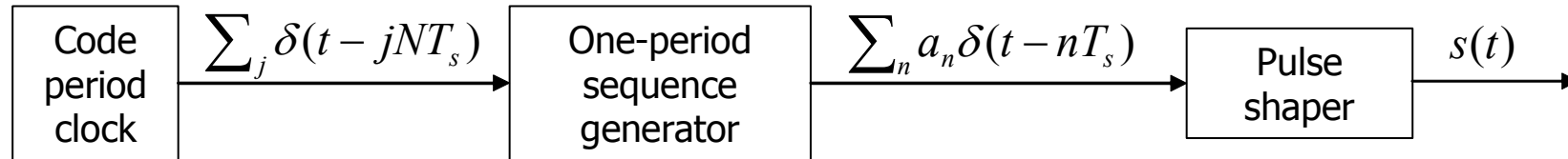
- $n = 8$: $(256, 255, 11, 15)$ -IRS $\mathbb{C} = \{X^{(1)}, X^{(2)}, \dots, X^{(16)}\}$
 - $\lambda_a = \max_i \max_{\tau \neq 0} R_{i,i}(\tau)$
 - $\lambda_c = \max_{i \neq j} \max_{\tau} R_{i,j}(\tau)$



【Fig. 4】 Autocorrelation profile of $X^{(4)}$ by type I construction (n=8)



【Fig. 5】 Maximum normalized crosscorrelation between $X^{(4)}$ and other sequences



[Fig. 6] Mathematical Model of a UWB signal generator without data modulation

● PSD calculation

- UWB carrier in simple form: $s(t) = \sum_n a_n p(t - nT_s)$ (N =the period of $\{a_n\}$, $N = N_s N_f$)

- $h_{op}(t) = \sum_{n=0}^{N-1} a_n \delta(t - nT_s)$, $H_{op}(f) = FT\{h_{op}(t)\} = \sum_{n=0}^{N-1} a_n e^{-j2\pi f n T_s}$

- $PSD_{cpc}(f) = \frac{1}{(NT_s)^2} \sum_k \delta\left(f - \frac{k}{NT_s}\right)$

- $PSD_s(f) = |P(f)H_{op}(f)|^2 PSD_{cpc}(f) = \frac{|P(f)|^2}{(NT_s)^2} \sum_k C_k \delta\left(f - \frac{k}{NT_s}\right)$

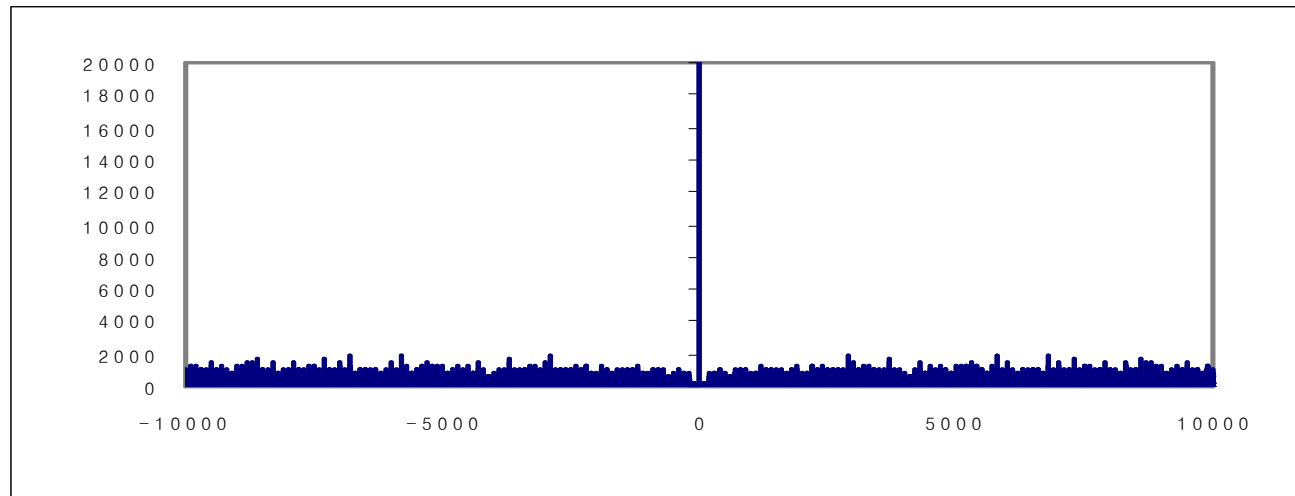
- $C_k = \left| \sum_{n=0}^{N-1} a_n e^{-j2\pi kn/N} \right|^2$: the effect of code design



Power Spectral Density (PSD) — (2)



- Spectral flatness (*Cancelation of Energy Spark*)
 - The flatter the PSD of the transmission, the larger the amount of power that can be radiated while still satisfying PSD bounds imposed by regulatory agencies.
 - Code for perfectly flat PSD
 - ▶ Codes from cyclic difference set
 - ▶ Not applicable to IRS because of "pulse position property"
- PSD of proposed IRS



【Fig. 7】 $C_k^{(4)}$ of type I construction (with peak value 65280 at $k = 0$)



Conclusion



- Time-hopping signal model and correlation consideration
 - ▶ NOT conventional BUT OOC (Optical Orthogonal Code) like correlation
 - ▶ Crosscorrelation with arbitrary time delay in slot time units as well as frame duration units
- **Design goal** of time-hopping code for UWB Impulse Radio
 - : to construct a signal set with
 - **Low correlation** for better performance of multiple access
 - **Spectral flatness** for efficient radiation of power
 - **Long period** for low PSD (energy spark cancellation)
 - **Easy generation** for system implementation
 - **Large number of sequences** to support as many users as possible
- Proposed design example has the features:
 - Very easy generation
 - For given parameter N_s , relatively long period
 - Improvement in correlation measure (compared to existing designs)
 - Usually flat PSD, but room for analysis and development



Future Directions



- Code design
 - Improvement of proposed design
 - New design using q -ary integer codes having good hamming correlation

- Consideration of known IRSs with optimal correlation
 - PSD analysis
 - Simulation with various modulation schemes